

Fibrin Clot Extension on Zirconia Surface for Dental Implants: A Quantitative In Vitro Study

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ABSTRACT

Purpose: The surface chemical and physical properties of materials used for implants have a major influence on blood clot organization. This study aims to evaluate the blood clot extension (*bce*) on zirconia and titanium. *bce* was measured in association to surface roughness (*Ra*) and static contact angle (θ).

Materials and Methods: Forty disk-shaped samples of sandblasted yttria tetragonal zirconia polycrystal (*sb-YTZP*), machined titanium (*m-Ti*), and sandblasted, high-temperature, acid-etched titanium (*p-Ti*) were used in the present study. About 0.2 mL of human blood, immediately dropped onto the specimen's surface and left in contact for 5 minutes at room temperature, was used to measure the *bce*. Specimens were observed under confocal scanning laser and scanning electron microscopes.

Results: The *bce* (mean $\times 10^7 \pm$ standard deviation [SD] $\times 10^6 \mu\text{m}^2$) was 2.97 ± 6.68 for *m-Ti*, 5.64 ± 6.83 for *p-Ti*, and 3.61 ± 7.67 for *sb-YTZP*. *p-Ti* samples showed a significantly higher *bce*. *Ra* (mean \pm SD [μm]) was 0.56 ± 0.7 for *m-Ti*, 3.78 ± 0.8 for *p-Ti*, and 2.68 ± 0.6 for *sb-YTZP*. The difference was not significant between *sb-YTZP* and *p-Ti*. θ (mean \pm SD) was 55.6 ± 5.6 for *m-Ti*, 48.7 ± 2.8 for *sb-YTZP*, and 38.0 ± 2.2 for *p-Ti*. The difference was not significant between *m-Ti* and *sb-YTZP*.

Conclusions: The *sb-YTZP* demonstrated a significantly lesser amount of *bce* compared with *p-Ti* specimens, notwithstanding that any significant difference was present between *Ra* and θ .

KEY WORDS: blood–material interaction, dental/endosteal implant, fibrin, surface characterization

INTRODUCTION

Dental implants are exposed, after insertion, to the patient's blood; the interactions of the foreign implant material with the implant surface will influence the extent of the fibrin network formation and of the acute inflammatory processes.^{1,2} Implant surface topography in the nanoscale to microscale will positively affect the reactions of the peri-implant bone³ and the bone growth processes.⁴ Chemistry and topography of dental implant

surfaces were able to influence interactions with all blood components.^{5,6} Osseointegration might, then, be directly influenced by the physicochemical properties of the implant surface.^{5,7} Titanium is the material of choice for dental implants and has also been reported to be highly thrombogenic.⁸ Because of the material's tooth-like color and its biocompatibility, yttria tetragonal zirconia polycrystal (YTZP) has become an attractive alternative to titanium for implants.^{9–12} YTZP is a bioinert material and shows minimal ion release compared with metallic implants. Recently, Özkurt and Kazazoglu¹³ in a literature review reported YTZP as an alternative materials for dental implants; Oliva and colleagues¹⁴ considered zirconia a viable alternative material for dental implants on the basis of a human clinical trial on eight hundred thirty-one zirconia dental implants with different roughness surfaces. Several authors have studied the factors related to surface properties, such as surface roughness, chemistry, and surface

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morphology.^{15–19} The ideal surface topography is, however, still unknown.¹⁵ The sensitivity of the cytoskeleton to organize in relationship to the surface microstructure seems to be high with an intermediate level of roughness and low in relatively smooth and extremely rough surfaces.¹⁷ In 2003, Kim and colleagues²⁰ evaluated the response of the peri-implant bone in blasted and blasted/etched implants: a higher quantity of bone in contact with blasted/etched implants in the primary healing period, while, after 3 months, no significant differences were found between the two groups. The same authors also suggested that with blasting and blasting/etching procedures, it would be possible to obtain implant surfaces with different roughnesses and oxide thicknesses.²⁰ Di Iorio and colleagues²¹ reported a significant fibrin clot retention for titanium implants with a microstructured surface. Sul and colleagues²² highlighted the importance of the oxide thickness for the bone reactions; they found that an oxide thickness of 600 to 1000 nm allowed a better bone-to-implant surface reaction. Buser and colleagues²³ and Larsson and colleagues²⁴ stated that bone-to-metal contact improved as implant surface becomes rougher. Nygren and colleagues²⁵ and Keselowsky and colleagues¹⁶ reported that, within a short time of contact, host plasma proteins were adsorbed on the implant surface. This biofilm, formed by immunoglobulins, vitronectin, fibrinogen, and fibronectin, seems to function as cell-adhesion-promoting and cell-activating ligands.¹⁶ Other studies^{26,27} underlined the relationship between the surface properties of the titanium and the adsorbed protein layer. Sevastianov²⁸ reported that albumin was adsorbed on the surface, while Tang and Eaton²⁹ showed that adsorbed fibrinogen played a relevant role in the activation of the inflammatory response of the bone tissue. When the plasma proteins contact the metal surface, there is an activation of the protein cascade, i.e., coagulation, fibrinolysis, and complement system.^{30–34} The coagulation is the first step of bone healing. Fibrinogen is the soluble blood precursor of the fibrin clot.³⁵ Both fibrinogen and fibrin are important in the clot formation, cellular and matrix interactions, fibrinolysis, inflammation, and wound healing.³⁵ Fibrin, formed at the site of injury, provides the temporary matrix, supporting the initial endothelial cell response for vessel repair.³⁶ Formation of a thrombus on biomaterials has been reported to be correlated with charge transfer from the inactive state of fibrinogen to the surface of the

biomaterial³⁷; fibrinogen tends to decompose to fibrin monomer and fibrinopeptides. The monomers will produce fibrin, before cross-linking to an irreversible thrombus. Moreover, it has been proven that fibrinogen had an electronic structure similar to an intrinsic semiconductor with a band gap of 1.8 eV,³⁷ and when fibrinogen was adsorbed onto the titanium oxide film, a junction was formed by the transfer of electrons, improving the blood biocompatibility. Over zirconia, this process was less effective because the band gap was >5 eV. Titanium has three types of oxide crystal structure: (1) anatase, (2) rutile, and (3) brookite. The band gap value for the anatase type is 3.20 eV, for the rutile type is 3.02 eV, and for the brookite type is 2.96 eV.³⁸ Fibrin is a material rapidly invaded, remodeled, and replaced by a cell-associated proteolytic activity.³⁹ The fibrin structure is quite loose at the beginning of the process, but after 5 minutes, a tighter structure will be formed under the influence of factor XIII (fibrin-stabilizing factor), converting the fibrin monomer into a polymer.⁴⁰ The formation of a fibrin scaffold is crucial because it represents the pathway that helps the osteogenic cells to reach the implant surface⁴¹; the osteogenic cells will not interact with the titanium implant surface, but with a blood-modified titanium oxide surface.⁴² According to the knowledge of the present authors, no information was present in the dental literature on the relationship between zirconia and fibrin clot.

The aim of the present study was a quantitative evaluation of the *in vitro* fibrin clot extension on zirconia and different titanium surfaces.

MATERIALS AND METHODS

General Procedure

A total of 43 disk-shaped specimens presenting a diameter of 5 mm and a thickness of 2 mm were used in the present study. Three different surface topographies and two types of implant materials were investigated. The specimens were divided as follows: 11 titanium specimens with machined surface (*m-Ti*) (DENTSPLY Implants Manufacturing GmbH, Mannheim, Germany); 11 titanium specimens with plus® surface (*p-Ti*) (DENTSPLY Implants Manufacturing GmbH); and 21 YTZP specimens with grit-blasted surface (*sb-YTZP*) (Diazir, Diadem SAS, Louey, France). The *m-Ti* specimens were obtained with a turning procedure (Figure 1); *p-Ti* disks were grit blasted with large grit

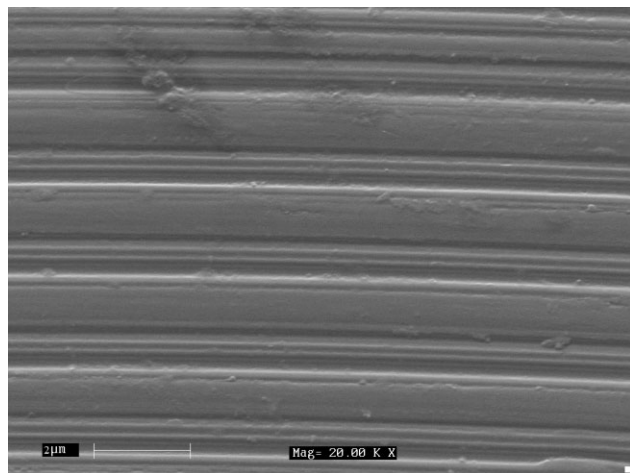


Figure 1 Scanning electron microscope image ($\times 20,000$) of machined titanium surface (*m-Ti*).

aluminum oxide particles (350–500 μm) and acid etched in high-temperature computer-controlled processes. The specific process used to produce the plus surface was considered a company proprietary process (Figure 2); the *sb-YTZP* specimens were obtained with a grit-blasting procedure with aluminum oxide particles (250–500 μm) at 5 bars followed by cleaning procedure in an ultrasonic bath containing 96% ethanol for 10 minutes (Figure 3).

Surface Characterization

A Zeiss confocal laser scanning microscope (CLSM) 510 META (Zeiss, Jena, Germany) using a 15-mW argon laser with a 40 \times / 1.2 finite numerical aperture (NA) objective and a 166- μm pinhole, was used to numerically describe the appearance of the surface topography.

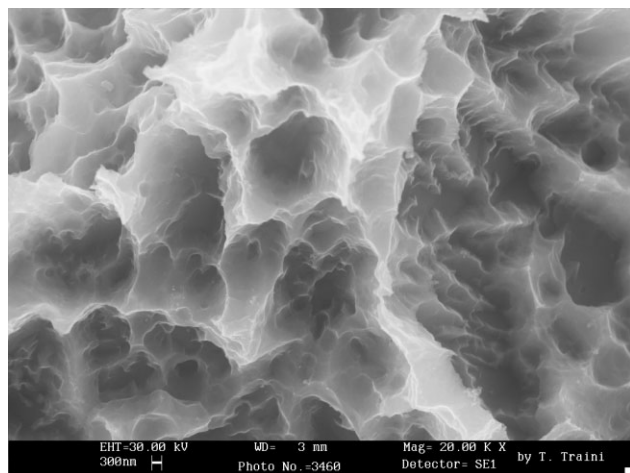


Figure 2 Scanning electron microscope image ($\times 20,000$) of plus titanium surface (*p-Ti*).

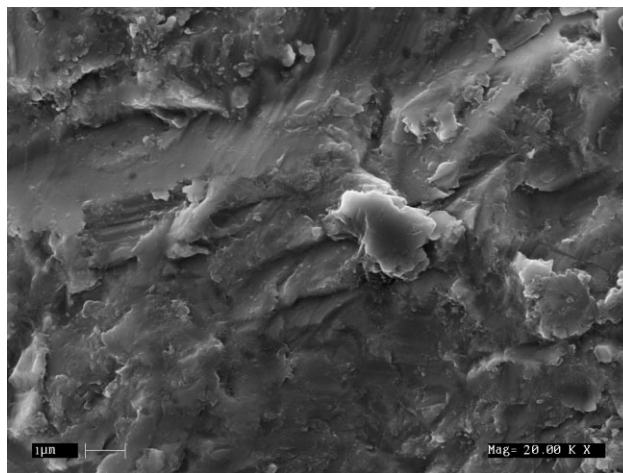


Figure 3 Scanning electron microscope image ($\times 20,000$) of sandblasted zirconia surface (*sb-YTZP*).

Three specimens for each of the three different surfaces were evaluated, while the area of measurement was 20 \times 20 μm . The surface parameter evaluated was the average height deviation value (*Ra*).

Contact Angle Measurements

Contact angles (θ), i.e., the angle between the tangent to a water drop and the solid surface at the three-phase liquid : solid : air meeting point,⁴³ were analyzed for each ($n = 3$) of the three different surfaces considered in the present study. The static contact angle was used as a measure of surface hydrophobicity. Sessile water drops with a volume of 10 μL were placed at the flat material surfaces under the same environmental conditions. The contact angle with water was measured from photographs, using Image-Pro Plus version 6.0 (Media Cybernetics Inc., Bethesda, MD, USA).

Blood Samples

Venous blood was drawn, with permission, from three adult healthy volunteers not on medication and with a bleeding time comprised between 2 and 3 minutes (Duke's assay). For all specimens, the human whole blood, without any addition of anticoagulant, was immediately dropped (0.1 mL) onto the surface of each specimen using a syringe. As blood drawn was instantly used for the experiment, the first drops were not discarded. About 0.1 mL of blood was sufficient to cover the entire specimen surface. Contact time was 5 minutes at room temperature; thereafter, the samples were rinsed with saline solution and fixed in a buffered solution

at pH 7.2 of 2.5% of glutaraldehyde and 2.5% of paraformaldehyde. Samples were washed again with buffer and dehydrated in an ascending alcohol series.

Measurements of Blood Clot

Samples belonging to the three different groups ($n = 25$) were investigated under both CLSM and scanning electron microscope (SEM).

For SEM surface characterization and measure, the specimens underwent critical point drying in Emitech K 850 (Emitech Ltd., Ashford, Kent, UK) than were mounted onto aluminum stubs, sputter gold coated in Emitech K 550 (Emitech Ltd.), and imaged in a Cambridge Stereoscan 200 (Cambridge Instrument Company Ltd, Cambridge, England) equipped with tetra-solid-state detector for back-scattered electrons (BSEs). The BSE signal was used because it is generated from about a 0.5- μm -thick surface layer of the specimen and because the number of emitted electrons was strongly dependent on the atomic number of the specimen. SEM operating conditions included 15- to 30-kV accelerating voltage, 14- to 32-mm working distance, and 0.75-nA probe current. The BSE images were captured with nine scans using a line average technique.

From each sample, 10 random micrographs at a magnification of $\times 1000$ were collected in .tif format with $N \times M$ (1024×768) grid of pixels. To measure the areas covered by the fibrin clot, the images were analyzed using Image-Pro Plus 6.0. To ensure accuracy, the software was calibrated for each experimental image using a software feature named "Calibration Wizard," which reports the number of pixel between two selected points (diameter of the disks). The linear remapping of the pixel numbers was used to calibrate the distance in microns. The measurements were drawn in square micrometer; individual average values were calculated

per sample, then, group average values were calculated, summarizing the individual values.

Statistics

One person performed all of the measurements. Carrying out two measurements for each index controlled intra-examiner variability. When the difference in the two performed readings exceeded 5% for the same index, the measure was repeated. Statistical analysis was performed by means of a computerized statistical package (Sigma Stat 3.5, SPSS Inc., Ekrath, Germany). The data were analyzed with descriptive statistics to assess whether they had a normal distribution. One-way analysis of variance (ANOVA) and Holm-Sidak tests were used to evaluate the overall significance and to perform all pairwise comparisons of the mean responses, respectively. A p -value of $<.05$ was considered statistically significant.

RESULTS

Under SEM, the *m-Ti* samples (Figure 1) showed the presence of typical machining grooves produced by the manufacturing instruments. The *p-Ti* samples (Figure 2) showed the presence of a macroscopic level of roughness in the dimensions of 100 μm . There was also a second level of grooves of about 20 to 70 μm ; these grooves were set around smaller grooves with different shapes. These second- and third-level grooves appeared to have very sharp edges. The *sb-YTZP* samples (Figure 3) showed a rough surface produced by the blasting procedure. The surface was irregular with many depressions, peaks, and small diameter indentations.

The surface roughness (R_a), measured under CLSM (Figure 4, A–C), was $0.56 \pm 0.7 \mu\text{m}$ for *m-Ti*, $2.68 \pm 0.6 \mu\text{m}$ for *sb-YTZP*, and $3.78 \pm 0.8 \mu\text{m}$ for *p-Ti*. The differences appeared to be statistically significant

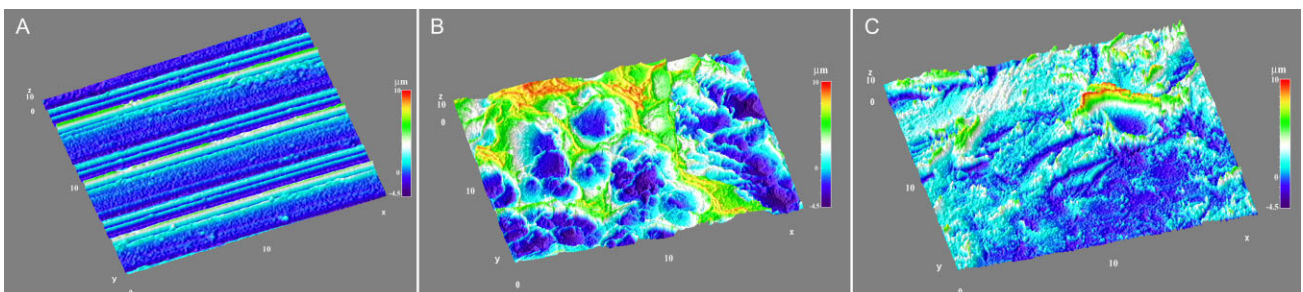


Figure 4 Three-dimensional reconstructions of surface topographies from R_a values under confocal laser scanning microscope. (A) *m-Ti* specimen; (B) *p-Ti* specimen; and (C) *sb-YTZP* specimen.

TABLE 1 Surface Roughness of Tested Materials (Mean ± SD)			
Groups	n	Ra (μm)	SD (μm)
m-Ti	3	0.56*	0.7
p-Ti	3	3.78*†	0.8
sb-YTZP	3	2.68*†	0.6

*Statistically significant.

†Not statistically significant at $\alpha < 0.05$ and $1 - \beta = 0.970$.

One-way ANOVA and Holm-Sidak methods.

ANOVA = analysis of variance; m-Ti = titanium specimens with machined surface; p-Ti = titanium specimens with plus surface; sb-YTZP = yttria tetragonal zirconia polycrystal specimens with sand-blasted surface; SD = standard deviation.

between both *p-Ti* and *sb-YTZP* versus *m-Ti* ($p < .05$), while no statistically significant difference was seen between *p-Ti* and *sb-YTZP* ($p > .05$) (Table 1).

The contact angles (θ), measured in static conditions (Figure 5, A–C), was 55.66 ± 5.6 for *m-Ti*, 38.00 ± 2.2 for *p-Ti*, and 48.70 ± 2.8 for *sb-YTZP*. Between *m-Ti* and *sb-YTZP*, no statistically significant difference was seen ($p > .05$), while for the *p-Ti* group, a significant decrease of θ ($p < .05$) was present (Table 2).

Quantitative analysis of blood clot extension (*bce*) (Figure 6) showed the following results: in *m-Ti* samples, *bce* was $2.97 \times 10^7 \pm 6.68 \times 10^6 \mu\text{m}^2$; in *p-Ti* samples, *bce* was $5.64 \times 10^7 \pm 6.83 \times 10^6 \mu\text{m}^2$; while in *sb-YTZP* samples, *bce* was $3.61 \times 10^7 \pm 7.67 \times 10^6 \mu\text{m}^2$. ANOVA discovered a significant difference among the groups ($p < .001$). The Holm-Sidak multiple comparison procedure revealed that the *bce* of *p-Ti* samples was statistically higher compared with both *m-Ti* and *sb-YTZP* samples ($p < .05$). No significant difference was noted between *m-Ti* and *sb-YTZP* samples ($p > .05$) (Table 3). SEM image comparison among all groups of samples showed also qualitative differences in *bce* organization. SEM images of *m-Ti* sample (Figure 7) showed a thin fibrin scaffold attached to the specimen surface

TABLE 2 Contact Angles (θ) of Tested Materials (Mean ± SD)			
Groups	n	Mean (°)	SD (°)
m-Ti	3	55.66*†	5.6
p-Ti	3	38.00*	2.2
sb-YTZP	3	48.70*†	2.8

*Statistically significant.

†Not statistically significant at $\alpha < 0.05$ and $1 - \beta = 0.965$.

One-way ANOVA and Holm-Sidak methods.

ANOVA = analysis of variance; m-Ti = titanium specimens with machined surface; p-Ti = titanium specimens with plus surface; sb-YTZP = yttria tetragonal zirconia polycrystal specimens with sand-blasted surface; SD = standard deviation.

with some red blood cells attached but not trapped by the fibrin filaments. Moreover, part of the specimen surface was visible and the fibrin scaffold appeared to be two dimensional. The *sb-YTZP* specimen (Figure 8), on the other hand, despite a tridimensional organization of the fibrin scaffold, showed only very few red blood cells trapped in the fibrin scaffold. Finally, the *p-Ti* specimen (Figure 9) demonstrated a very intricate tridimensional organization of the fibrin scaffold with some red blood cells attached and trapped by the implant surface microconcavities.

DISCUSSION

Hemocompatibility is a key factor in the successful design and function of a medical device. When a foreign material comes into contact with blood, changes occur in both the hemostatic and inflammatory systems.^{25,44} Thus, it should not be surprising that the adhesion of cells to biomaterial surfaces is a crucial step in the tissue/biomaterial integration.¹⁶ This adhesive interaction anchors cells that activate several intracellular signaling pathways to direct cell viability, proliferation, and differentiation.¹⁶ The tissue response to rougher surfaces seems to be better than that observed around smoother

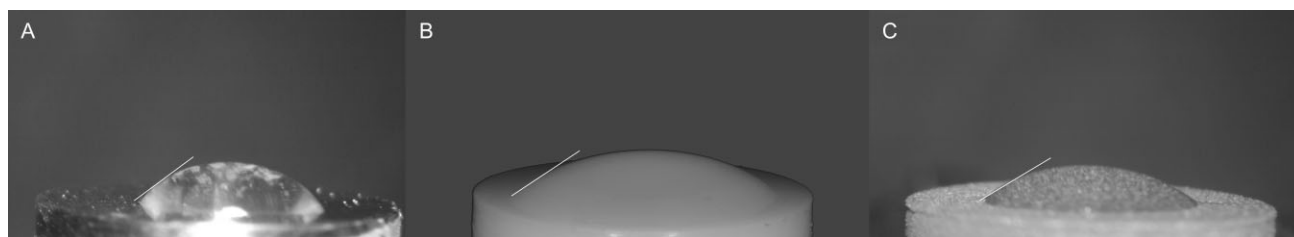


Figure 5 Measure of the surface hydrophobicity (contact angles) by sessile water drops. (A) *m-Ti* specimen; (B) *sb-YTZP* specimen; and (C) *p-Ti* specimen.

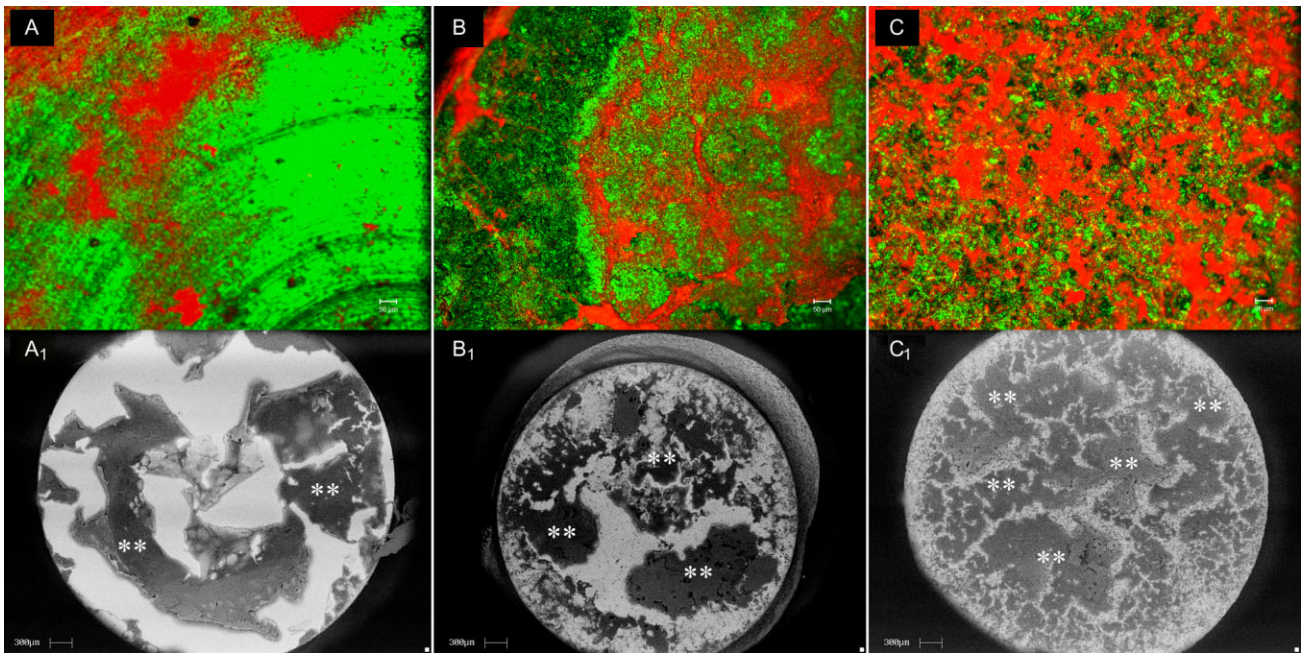


Figure 6 Evaluation of blood clot extension (*bce*). Under confocal laser scanning microscope ($\times 200$), *bce* appeared in red and the specimen surface in green. (A) *m-Ti* specimen; (B) *sb-YTZP* specimen; and (C) *p-Ti* specimen. Under scanning electron microscope image ($\times 37$) using back-scattered electrons, *bce* (**) appeared black-gray and specimen surface in gray-white. (A₁) *m-Ti* specimen; (B₁) *sb-YTZP* specimen; and (C₁) *p-Ti*.

ones,¹⁵ probably due to an increase of the surface area available for adhesion.¹⁵

The present study clearly demonstrated that implant surface roughness has an important role for early biomaterial integration. The hierarchical structure of the *p-Ti* samples, observed under SEM, resulted in a microporous topography surface able to literally catch the red blood cells. These findings were consistent with a previous report.²¹ The present results also suggested that the type of material was able to influence the activation

of the common pathways of blood coagulation and of platelet activation. The changes in blood coagulation in this study could be directly correlated to the changes in the surface chemistry induced by the material type. This was evidenced by the difference in contact angle from 48.70° for *Sb-YTZP* down to 38.00° for *p-Ti*.

The statistically significantly higher amount of fibrin clot on the *p-Ti* surface than on the *sb-YTZP* or

TABLE 3 Blood Clot Extension on Sample Surfaces			
Groups	<i>n</i>	Means ($\times 10^7 \mu\text{m}^2$)	Standard Deviations ($\times 10^6 \mu\text{m}^2$)
<i>m-Ti</i>	5	2.97* [†]	6.68
<i>p-Ti</i>	5	5.64*	6.83
<i>sb-YTZP</i>	15	3.61* [†]	7.67

*Statistically significant.

[†]Not statistically significant at $\alpha < 0.05$ and $1 - \beta = 1.00$.

Normality test: passed ($p = .489$); equal variance test: passed ($p = .988$). One-way ANOVA and Holm-Sidak methods.

ANOVA = analysis of variance; *m-Ti* = titanium specimens with machined surface; *p-Ti* = titanium specimens with plus surface; *sb-YTZP* = yttria tetragonal zirconia polycrystal specimens with sand-blasted surface.

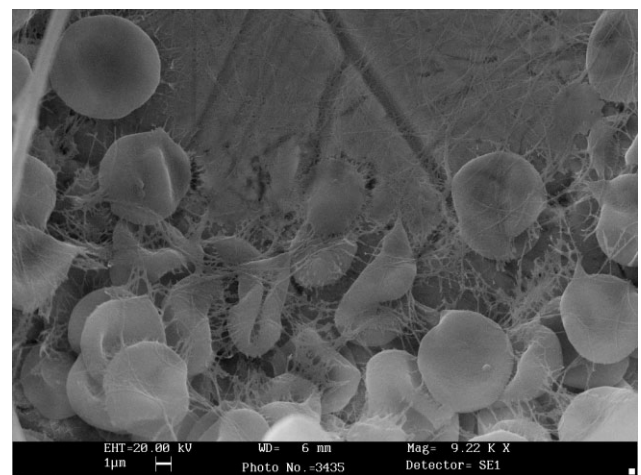


Figure 7 Scanning electron microscope image ($\times 9,220$) of machined titanium surface (*m-Ti*) with blood clot. Fibrin filaments are thin and not very extensive; some red blood cells are also visible.

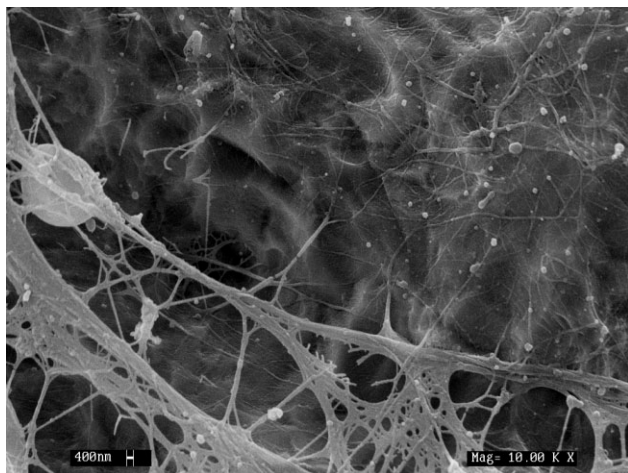


Figure 8 Scanning electron microscope image ($\times 10,000$) of sandblasted zirconia surface (*sb-YTZP*) with blood clot. The fibrin scaffold looks like a three-dimensional network; the zirconia surface is visible in the background; two red blood cells trapped in the fibrin scaffold are also visible.

m-Ti surfaces appeared to be related to the three-dimensional arrangement of the fibrin clot among the groups. In the *m-Ti* group, the fibrin network had a two-dimensional extension, with large areas of the metal surface visible among the fibrin filaments (Figure 7), while in the *p-Ti* group, the fibrin appeared like a three-dimensional network (Figure 9). The microscopic morphology of the fibrin clot on the *sb-YTZP* samples appeared to be interesting, which showed very few red blood cells retained inside the three-dimensional fibrin scaffold (Figure 8). It was hypothesized that the implant

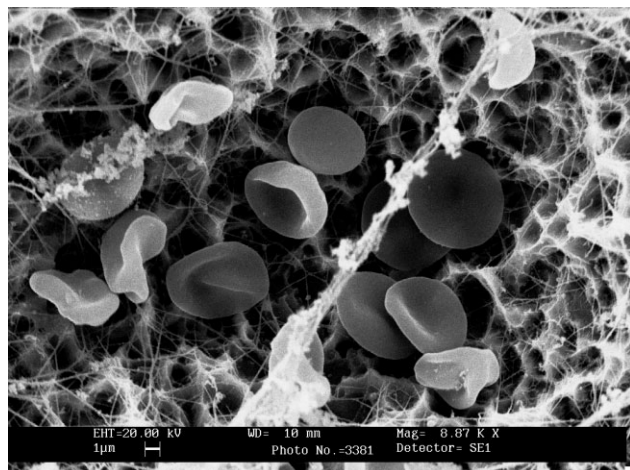


Figure 9 Scanning electron microscope image ($\times 8,870$) of plus titanium surface (*p-Ti*) with blood clot. Both fibrin and red blood cells are present. A three-dimensional extensive intricate fibrin network is visible on specimen surface with red blood cells trapped in the fibrin scaffold.

surface microtexture could influence the spatial arrangement of the fibrin while the electronic structure of the material surface was able to influence the chemistry of the coagulation. In fact, the band gap of the zirconia was >5 eV, while the band gap value of titanium was 3.06 ± 0.12 eV, much closer to 1.8 eV of fibrinogen. In some ways, the coagulation process was less effective over the zirconia samples. Comparing the results for *bce* and contact angles (Figure 10), the inverse relation between contact angle and *bce* was evident. *sb-YTZP* showed a higher contact angle and a lower *bce* value. The *bce* value of *sb-YTZP* was slightly more than *m-Ti* and the *Ra* values of the two groups were significantly different. The higher amount of fibrin and the large number of red blood cells should be related to the rate of platelet activation during clot formation, due to a major amount of chemotactic factors released in healing site.⁴²

According to Park and Davies,⁴⁵ the agglomeration of red cells could be caused by the release of macromolecules by platelets; hence, the presence of red cells could be caused by the activation of platelets. The fibrin three-dimensional structure on the *p-Ti* surface could be related both to the three-dimensional microstructure of this surface and to the closer band gap energy with fibrinogen. Further studies are, however, necessary to clarify this point. As described by Davies,⁴¹ bone healing around dental implants could be divided in osteogenic cell migration, de novo bone formation, and bone remodeling. Osteogenic cell migration and de novo bone formation were two phases of the same process named “contact osteogenesis,” with formation of bone directly on the implant surface. The first step of contact osteogenesis was the recruitment of osteogenic cells from perivascular connective tissue; these cells could migrate toward the implant surface using the fibrin scaffold. Interactions between membrane proteins and fibrin were crucial in producing the ameboid movements through the fibrin scaffold. These mechanisms stressed the importance of the fibrin scaffold in the early phases of healing of peri-implant bone. The ability of the implant surface to retain the fibrin attachment during the wound contraction seemed to be of relevant importance in maintaining the pathway for the osteogenic cells to reach the implant surface.⁴¹

The type, quantity, and activity of adsorbed proteins were influenced by the properties of the biomaterial (surface chemistry and hydrophobicity).^{16,46} *p-Ti* surface has been shown to be totally wettable after the first

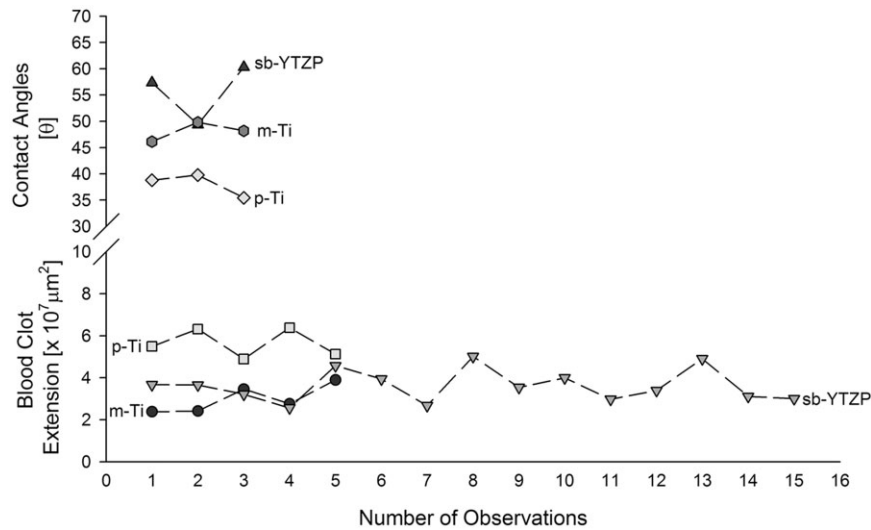


Figure 10 Plot of contact angles *versus* blood clot extension (*bce*). The inverse relation between contact angle and *bce* appear evident. *sb-YTZP* shows both a high-contact angle and a low-*bce* rate. *p-Ti* and vice versa show a low-contact angle and a high-*bce* rate.

emersion cycle.⁴⁶ It was hypothesized that there could be a direct correlation of the hierarchical structure of indentations of the *p-Ti* surface and the wetting behavior.⁴⁶ Moreover, the presence of the sharp edges observed under SEM on the *p-Ti* surface (Figure 2) could help the adhesion of cells by presenting a differential in the chemistry of the implant surface.¹⁹ The proteins adsorbing to the edge could take up a different shape from those adsorbed to a continuously flat surface.¹⁹

According to Johnson and colleagues,⁴⁴ whole blood instead of anticoagulated blood was used in the present study because anticoagulation substances could modify the blood coagulation cascade.

In conclusion, the results of this *in vitro* study revealed that the *sb-YTZP* specimens showed, in mean, a significant decrease of *bce* compared with *p-Ti* specimens, while the values of both *Ra* and θ were not statistically different. The increase of the surface microtexture complexity as well as the use of titanium seemed both to determine the formation of a more extensive and three-dimensionally complex fibrin scaffold. Further investigations are necessary to explain the relationships between band gap energy and blood clot formation.

DISCLOSURE

The authors have not received remuneration or other perquisites for personal or professional use from a commercial or industrial agent in direct or indirect relationship to their authorship.

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