The Wetting of Surface-Treated Silicone Impression Materials by Gypsum Mixes **Containing Disinfectants and Modifiers**

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Purpose: This work evaluated wettability of silicone impression surfaces by gypsum mixes containing disinfectants.

Materials and Methods: Two types of dental stone were modified by mixing with aqueous solutions of either sodium hypochlorite or povidone iodine. These materials were subjected to further modification by adding a mixture of 1% gum arabic and 0.132% calcium hydroxide to reduce the water requirement of the hemihydrate. Mix consistency tests were carried out to determine the effect of the disinfectants and the modifying additives on the mix fluidity. Contact angles of the mixed materials were measured when they were poured against a polyvinylsiloxane impression material that had undergone the following treatments (1) no treatment (control), (2) surfactant treated, (3) disinfectant treated, and (4) treated with both surfactant and disinfectant. One-way analysis of variance (ANOVA) was carried out using Dunnett's method to determine if experimental groups were significantly different from the control.

<u>Results:</u> Gypsum mix consistency was reduced by the presence of combined gum arabic and calcium hydroxide additives. Contact angle data showed that the additives and disinfectants incorporated into the gypsum had, in general, no beneficial effect on the wetting of an untreated silicone surface, or a surface treated with surfactant. In some instances, better wetting was obtained with disinfectanttreated surfaces, and surfaces that had been disinfected and treated with surfactant.

Conclusions: Fluidity of the mixed gypsum was affected by the modifying additives. Chemical disinfectants incorporated in gypsum have little effect on the wetting behavior of dental gypsum. Modifying dental stone powders with gum arabic and calcium hydroxide additives (before mixing at the manufacturers' recommended liquid/powder ratios), improved the wetting behavior of the mixed materials in some cases, but results were not consistent.

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POSSIBLE TRANSMISSION of pathogenic microorganisms by means of dental impressions and cast and die materials is of great concern for dental office and laboratory personnel. In previous

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research, the effect of disinfecting additives on dental gypsum has been studied, in terms of bulk mechanical properties¹ and surface properties.² Such additives can be used in conjunction with a mixture of added calcium hydroxide and gum arabic, which serves to reduce the water requirement of the gypsum.¹⁻⁴

The interaction between mixed gypsum and impression materials is important. Certain impression materials appear to yield stone casts that contain more entrapped air bubbles than others using the same die stone.¹ Many of the earlier versions of addition silicone impression materials produced hydrogen gas on setting.

Poor wettability of impression materials, as measured by contact angle analysis, is also considered a factor contributing to negative surface defects or voids in stone casts. It has been shown

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that the greater the contact angle, the greater the probability of formation of surface defects in stone casts.²

Thus, some manufacturers have produced hydrophilic impression materials by the incorporation of a surfactant.⁵ The wettability of elastomeric impression materials can also be increased by application of a surface tension reducing agent (topical surfactant) to the set impression before pouring.⁶

The present work was undertaken to explore the hypothesis that the wettability of a polyvinylsiloxane (PVS) impression material will be affected by (1) surfactant treatment of the impression material and (2) by the presence of disinfectants—both with and without water-reducing additives—in the gypsum mixes.

Materials and Methods

Materials

Two types of dental stone (Type III, Lab Stone, lot no. 25375; Type V, Die Keen, lot no. 46580; both from Heraeus Kulzer Inc, South Bend, IN) were mixed with an aqueous solution of chemical disinfectants, either 0.525% sodium hypochlorite (NaOCl) (Fox-Chlor, Fox Packaging Co, St. Paul, MN, lot no. 62207-6) or 0.1% povidone iodine (PI) (Betadine, The Purdue Frederick Co., Norwalk, CT, lot no. 0034-2100-01), in addition to water, which served as the control. Hemihydrate powders of these stones were subjected to further modification by adding both 1% gum arabic (lot no. 9000-01-5, Acros Organics, Fairlawn, NJ) and 0.132% calcium hydroxide (lot no. 792589, Fisher Scientific, Fairlawn, NJ) based on previous studies.^{3,4} The modified materials were mixed at the manufacturers' recommended liquid-powder (L/P) ratios (0.30 and 0.21 for types III and V, respectively) and at reduced L/P ratios (0.26 and 0.19 for types III and V stone, respectively). Table 1 shows the formulations of gypsum tested. There were 14 experimental groups, designated III.1 to III.7 and V.1 to V.7 for the type III and V stones, respectively.

Mix Consistency

Accurately proportioned amounts of dental stones and mixing solutions were hand mixed following ADA specification no. 25. The mixed material was then placed in a disposable plastic syringe to dispense five 2 ml quantities of material onto a glass plate, followed by vibration at high speed for 5 seconds (timed with a digital stopwatch), during which the mixed material flowed to form an approximately circular disk. The vibrator was Buffalo model number 1A (Buffalo Dental Mfg. Co. Inc, Syosset, NY), used at the high setting.

After setting, the diameter of each specimen was measured 3 times, in different directions, using a digital micrometer (Mitutoyo Solar, digimatic micrometer, Model CD-S6 CP, Mitutoyo Corp., Japan), and the mean diameters were calculated. A larger diameter indicated greater fluidity of the mixed material.

Wetting Behavior

Wetting behavior of the mixed materials was assessed against four differently treated polyvinylsiloxane (Imprint II, 3M ESPE Dental Products, St. Paul, MN) impression surfaces as follows:

 Untreated. Impression surfaces not subjected to any sort of treatment before pouring of mixed stones.

Table 1. Experimental Design*

Group	Dental Stone	Additives to Stone	Liquid	Liquid/Powder Ratio
III.1	Type III	None	Water	0.30
III.2	Type III	None	0.525% NaOCl	0.30
III.3	Type III	None	0.1% PI	0.30
III.4	Type III	1% gum arabic and 0.132% Ca(OH) ₂	0.525% NaOCl	0.30
III.5	Type III	1% gum arabic and 0.132% $Ca(OH)_{2}^{2}$	0.1% PI	0.30
III.6	Type III	1% gum arabic and 0.132% $Ca(OH)_{2}^{2}$	0.525% NaOCl	0.26
III.7	Type III	1% gum arabic and 0.132% $Ca(OH)_{2}^{2}$	0.1% PI	0.26
V.1	Type V	None	Water	0.21
V.2	Type V	None	0.525% NaOCl	0.21
V.3	Type V	None	0.1% PI	0.21
V.4	Type V	1% gum arabic and 0.132% Ca(OH) ₂	0.525% NaOCl	0.21
V.5	Type V	1% gum arabic and 0.132% $Ca(OH)_2$	0.1% PI	0.21
V.6	Type V	1% gum arabic and 0.132% Ca $(OH)_2$	0.525% NaOCl	0.19
V.7	Type V	1% gum arabic and 0.132% $Ca(OH)_2$	0.1% PI	0.19

*Each of the above 14 gypsum mixes was tested against the polyvinylsiloxane material under each of 4 conditions (1) no surface treatment of the impression material, (2) surfactant treatment, (3) treated with disinfectant, and (4) treated with disinfectant followed by the surfactant.

	Type III Stone					Type V Stone				
Group	Mean Disk Diameter (mm)			SD(n=5)	Group	Mean Disk Diameter (mm)			SD(n=5)	
III.1 III.2 III.3 III.4 III.5 III.6 III.7	$25.1 25.4 24.9 33.8* 40.6* 24.2 26.8 24.2 \\ 26.8 \\ 24.2 \\ 26.8 \\ 24.2 \\ 26.8 \\ 24.2 \\ 26.8 \\ 24.9 \\ 24.9 \\ 26.4 \\ 24.9 \\ 26.4 \\ 24.9 \\ 26.4 \\ 24.9 \\ 26.4 \\ 24.9 \\ 26.4$			$\begin{array}{c} 0.8 \\ 0.9 \\ 1.1 \\ 2.0 \\ 1.3 \\ 5.2 \\ 1.3 \end{array}$	V.1 V.2 V.3 V.4 V.5 V.6 V.7	$\begin{array}{cccccccccccccccccccccccccccccccccccc$			$ \begin{array}{r} 1.2 \\ 1.6 \\ 1.5 \\ 0.8 \\ 0.9 \\ 1.9 \\ 1.0 \\ \end{array} $	
		One-Way AN	OVA		One-Way ANOVA					
Source Model Error C Total	DF 6 28 34	Sum of sq 1153.2545 148.8358 1302.0903	Mean sq 192.209 5.316	F-ratio 36.1597 <i>P</i> -value <0.0001	Source Model Error C Total	DF 6 28 34	Sum of sq 1557.6612 49.3235 1606.9847	Mean sq 259.610 1.762	F-ratio 147.3758 <i>P</i> -value <0.0001	

 Table 2. Mix Consistency of Dental Stones

*Significantly different from control by Dunnett's test (p < 0.05).

- Surfactant treated. Impression surfaces were sprayed with topical surfactant (Delar Corporation, Lake Oswego, OR) before pouring of mixed stones.
- Disinfectant treated. Impression surfaces were spray disinfected with 0.525% NaOCl and air dried after 10 minutes, before pouring of mixed stones.
- Disinfected, surfactant treated. Impression surfaces were disinfected as previously described, then sprayed with topical surfactant before pouring of mixed stones.

Using a similar method to that of Lorren et al,⁷ five 2 ml disks of the mixed stones were dispensed over flat impression surfaces (18 cm \times 12 cm \times 3 mm), followed by vibration at high speed for 2 seconds. After setting, these disks were sectioned into 2 halves and their cross-section was seen at 10× original magnification using a computer-linked stereomicroscope (Olympus PM-PB20, Japan) and a video camera (Sony CCD-IRIS/RGB, Japan). All pictures were then captured and printed, in order to facilitate the protractor measuring of contact angles represented by the cross-sectional edges of each stone disk. The mean contact angle for each disk was then determined and the results were subjected to statistical analysis.

Statistical Analysis

One-way analysis of variance (ANOVA) was used for both consistency and wetting behavior data. Dunnett's method was used to determine which group(s) of mixed stones differed significantly from the control.

Results

A significant difference was detected for the mix consistency of each of type III and type V stone mixes (p < 0.0001 for both, Table 2). Type III stone materials modified with gum arabic and calcium hydroxide additives and mixed at the manufacturer's recommended L/P ratio showed a significantly lower consistency than the control mix (Dunnett's values = 4.71 and 11.54). Again, the gum arabic and calcium hydroxide-modified type V stone materials mixed at either the manufacturers' recommended or reduced L/P, all showed a significantly lower consistency than the control.

The contact angle data are presented in Tables 3-6 for the 4 differently treated silicone surfaces. Type III disinfected stones showed no difference in contact angle between the mixes and the control when all were poured against untreated impression surfaces (Table 3), while the unmodified type V stone mixed either with NaOCl or P.I. (Groups V.2 and V.3) showed higher contact angles when measured against the untreated impression surfaces. Contact angles of both types of stone (whether modified or not), differed from the control when measured against the surfactant-treated, disinfectant-treated, and disinfected surfactant-treated impression surfaces. The only clear exception is for the unmodified materials mixed with NaOCl (Tables 4-6).

Discussion

The clinical implication of this work is that it would be beneficial to have gypsum products with incorporated disinfectants as a passive means of control of cross-infection. This work has explored

	Type III Stone					Type V Stone					
Group	Con	tact Angle (Degr	rees)	SD(n=5)	Group	(Contact Angle (D	egrees)	SD(n=5)		
III.1 III.2 III.3 III.4 III.5 III.6 III.7		$\begin{array}{c} 67.0 \\ 70.4 \\ 67.6 \\ 64.6 \\ 65.2 \\ 64.4 \\ 66.4 \end{array}$		$ \begin{array}{r} 1.6 \\ 2.6 \\ 1.1 \\ 2.9 \\ 2.9 \\ 1.1 \\ 2.3 \\ \end{array} $	V.1 V.2 V.3 V.4 V.5 V.6 V.7		$\begin{array}{c} 60.8 \\ 71.0^* \\ 65.4^* \\ 62.0 \\ 64.2 \\ 62.4 \\ 63.8 \end{array}$		2.4 2.0 1.7 2.9 1.9 1.5 1.5		
111.7	One-Way ANOVA				•.,		One-Way AN	IOVA	1.0		
Source Model Error C Total	DF 6 28 34	Sum of sq 131.94286 134.80000 266.74286	Mean sq 21.9905 4.8143		Source Model Error C Total	DF 6 28 34	Sum of sq 337.37143 116.80000 454.17143	Mean sq 56.2286 4.1714	F-ratio 13.4795 <i>P</i> -value <0.0001		

Table 3. Wetting Behavior of Stones Against Untreated Silicone Impression Surfaces

*Significantly different from control by Dunnett's test (p < 0.05).

this possibility by determining the ability of disinfected mixes to wet a polyvinylsiloxane material given different chemical treatments.

The consistency test was conducted to discover the effect of consistency on the wetting behavior of the mixed, disinfected stones against impression surfaces. Materials with low viscosity (consistency) will flow and spread readily over impression surfaces with gentle vibration, while others with high consistency could show reduced flow rates. A disk diameter test was selected because it is a simple, reliable, and easily controlled method, and it has been used in previous studies.⁴ In this study, aqueous solutions of chemical disinfectants had no significant effect on the consistency of the mixed dental materials; however, these consistencies were reduced by the addition of gum arabic and calcium hydroxide to the hemihydrate powders before mixing at the manufacturers' recommended L/P ratios. This reduction was the result of excess liquid content of the mixed materials, in agreement with the results of Alsadi et al.⁴

Surface defects on stone casts could affect the accuracy of cast restorations. Numerous factors can contribute to surface defects or void formation in stone dies, including production of hydrogen gas by many addition-cured silicone impression materials and poor wettability of impression materials. The greater the contact angle, the greater the probability of surface defects in stone casts.⁸ It has been shown that the ability of liquid to wet a solid surface is dependent on the surface tension of the liquid as well as the surface energy of the substrate,^{9,10} which is markedly affected by the application of a surface tension reducing agent.⁶

	Type III Stone					Type V Stone					
Group	Contact Angles (Degrees)			SD(n=5)	Group	Contact Angles (Degrees)			SD(n=5)		
III.1 III.2 III.3 III.4 III.5 III.6 III.7		$\begin{array}{c} 48.6 \\ 66.4^* \\ 60.2^* \\ 55.6^* \\ 47.8 \\ 57.0^* \\ 56.0^* \end{array}$		$2.7 \\ 1.5 \\ 1.5 \\ 2.1 \\ 2.8 \\ 1.6 \\ 1.9$	V.1 V.2 V.3 V.4 V.5 V.6 V.7		$57.0 \\ 63.8^* \\ 57.6 \\ 56.2 \\ 47.6^* \\ 55.4 \\ 55.4 \\ 55.4 \\ $		$2.3 \\ 2.6 \\ 2.5 \\ 1.8 \\ 1.5 \\ 2.1 \\ 1.7$		
	One-Way ANOVA						One-Way AN	IOVA			
Source Model Error C Total	DF 6 28 34	Sum of sq 1244.6857 119.2000 1363.8857	Mean sq 207.448 4.257	F-ratio 48.7293 <i>P</i> -value <0.0001	Source Model Error C Total	DF 6 28 34	Sum of sq 677.88571 124.40000 802.28571	Mean sq 112.981 4.443	F-ratio 25.4298 <i>P</i> -value <0.0001		

Table 4. Wetting Behavior of Stones Against Surfactant-Treated Silicone Impression Surfaces

*Significantly different from control by Dunnett's test (p < 0.05).

	Type III Stone					Type V Stone				
Group	Con	ntact Angle (Deg	rees)	SD(n=5)	Group	(Contact Angle (D	SD(n=5)		
III.1 III.2 III.3 III.4 III.5 III.6 III.7		$76.4 \\ 77.8 \\ 69.4^* \\ 62.2^* \\ 65.6^* \\ 66.6^* \\ 66.6^* \\ 66.6^* \\$		$1.1 \\ 0.8 \\ 2.9 \\ 3.3 \\ 2.3 \\ 2.3 \\ 3.0$	V.1 V.2 V.3 V.4 V.5 V.6 V.7		73.274.064.0*65.2*64.4*65.6*65.4*		$1.9 \\ 2.3 \\ 1.6 \\ 3.1 \\ 2.4 \\ 1.1 \\ 1.7$	
One-Way ANOVA					One-Way ANOVA					
Source Model Error C Total	DF 6 28 34	Sum of sq 1006.5714 163.6000 1170.1714	Mean sq 167.762 5.843	F-ratio 28.7123 <i>P</i> -value <0.0001	Source Model Error C Total	DF 6 28 34	Sum of sq 549.20000 125.20000 674.40000	Mean sq 91.5333 4.4714	F-ratio 20.4707 <i>P</i> -value <0.0001	

Table 5. Wetting Behavior of Stones Against Disinfectant-Treated Silicone Impression Surfaces

*Significantly different from control by Dunnett's test (p < 0.05).

Table 6. Wetting Behavior of Stones Against Disinfected, Surfactant-Treated Silicone Impression Surfaces

	Type III Stone					Type V Stone				
Group	Con	atact Angle (Degr	rees)	SD(n=5)	Group	Contact Angle (Degrees)			SD(n=5)	
III.1 III.2 III.3 III.4 III.5 III.6 III.7		$\begin{array}{c} 65.4 \\ 65.6 \\ 64.4 \\ 53.0^{*} \\ 52.2^{*} \\ 54.4^{*} \\ 53.8^{*} \end{array}$		3.4 2.2 2.1 1.2 2.2 3.5 1.3	V.1 V.2 V.3 V.4 V.5 V.6 V.7		$\begin{array}{c} 61.8\\ 65.6\\ 57.2^*\\ 51.2^*\\ 56.4^*\\ 53.6^*\\ 55.2^* \end{array}$		$2.8 \\ 3.0 \\ 1.9 \\ 2.6 \\ 1.1 \\ 2.4 \\ 0.8$	
One-Way ANOVA					One-Way ANOVA					
Source Model Error C Total	DF 6 28 34	Sum of sq 1208.0000 162.4000 1370.4000	Mean sq 201.333 5.800	F-ratio 34.7126 <i>P</i> -value <0.0001	Source Model Error C Total	DF 6 28 34	Sum of sq 726.34286 140.80000 867.14286	Mean sq 121.057 5.029	F-ratio 24.0739 <i>P</i> -value <0.0001	

*Significantly different from control by Dunnett's test (p < 0.05).

The contact angle is considered the best indicator of the wetting behavior of liquids against different substrates. Using the method recommended by Lorren et al⁷ also seems to be realistic, because it reflects the exact situation of pouring and measures the contact angle of the mixed stone itself, not a gypsum slurry, against the impression surface.

Not all disinfectants used in this study reduced the wetting behavior of dental stones, although most of the disinfected materials showed higher contact angles against different types of impression surface treatments. Therefore, the mixed materials spread less easily over impression surfaces. The 0.1% povidone iodine had possibly the lowest surface tension among the disinfectants considered, and that was reflected in the contact angles of stones mixed with this solution. Addition of gum arabic and calcium hydroxide reduced the liquid required for mixing and reduced the consistency of stones mixed at the manufacturers' recommended L/P ratios. This reduction in consistency helped the flow of the mixed materials over the impression surfaces. With reduction of the L/P mixing ratios, the effect of reduced consistency was mitigated, that is, the contact angle then returned to higher measurements.

Conclusions

- *1.* Fluidity of mixed gypsum could be affected in the presence of modifying additives.
- 2. Chemical disinfectants have little effect on the wetting behavior of dental gypsum.

3. Modifying dental stone powders with gum arabic and calcium hydroxide additives before mixing at the manufacturers' recommended L/P ratios improves the wetting behavior of the mixed materials.

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