



L. M. Gallo
L. R. Iwasaki
Y. M. Gonzalez
H. Liu
D. B. Marx
J. C. Nickel

Diagnostic group differences in temporomandibular joint energy densities

Authors' affiliations:

L. M. Gallo, Center of Dental Medicine, Clinic of Masticatory Disorders, Removable Prosthodontics, Geriatric and Special Care Dentistry, University of Zurich, Zurich, Switzerland

L. R. Iwasaki, H. Liu, J. C. Nickel, Departments of Orthodontics & Dentofacial Orthopedics, and Oral & Craniofacial Sciences, School of Dentistry, University of Missouri-Kansas City, Kansas City, MO, USA

Y. M. Gonzalez, Department of Oral Diagnostic Sciences, School of Dental Medicine, University at Buffalo, Buffalo, NY, USA

D. B. Marx, Department of Statistics, University of Nebraska-Lincoln, Lincoln, NE, USA

Correspondence to:

J. Nickel
Department of Orthodontics and
Dentofacial Orthopedics
School of Dentistry
University of Missouri-Kansas City
650 E. 25th Street
Kansas City, MO 64108, USA
E-mail: nickeljc@umkc.edu

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Structured Abstract

Objectives – Cartilage fatigue, due to mechanical work, may account for precocious development of degenerative joint disease in the temporomandibular joint (TMJ). This study compared energy densities (mJ/mm³) in TMJs of three diagnostic groups.

Setting and Sample Population – Sixty-eight subjects (44 women, 24 men) gave informed consent. Diagnostic criteria for temporomandibular disorders (DC/TMD) and imaging were used to group subjects according to presence of jaw muscle or joint pain (+P) and bilateral disk displacement (+DD).

Material and Methods – Subjects (+P+DD, $n = 16$; –P+DD, $n = 16$; and –P–DD, $n = 36$) provided cone-beam computed tomography and magnetic resonance images, and jaw-tracking data. Numerical modeling was used to determine TMJ loads (F_{normal}). Dynamic stereometry was used to characterize individual-specific data of stress-field dynamics during 10 symmetrical jaw-closing cycles. These data were used to estimate tractional forces (F_{traction}). Energy densities were then calculated as W/Q (W = work done or mechanical energy input = tractional force \times distance of stress-field translation, Q = volume of cartilage). ANOVA and Tukey–Kramer *post hoc* analyses tested for intergroup differences.

Results – Mean \pm standard error energy density for the +P+DD group was 12.7 ± 1.5 mJ/mm³ and significantly greater (all adjusted $p < 0.04$) when compared to –P+DD (7.4 ± 1.4 mJ/mm³) and –P–DD (5.8 ± 0.9 mJ/mm³) groups. Energy densities in –P+DD and –P–DD groups were not significantly different.

Conclusion – Diagnostic group differences in energy densities suggest that mechanical work may be a unique mechanism, which contributes to cartilage fatigue in subjects with pain and disk displacement.

Key words: cartilage; fatigue; human; mechanics; temporomandibular joint

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Introduction

The etiological variables that result in the precocious development of degenerative joint disease of the TMJ have yet to be elucidated. The biomechanical and biochemical integrity of articular tissue is likely to be dependent on the magnitude and frequency of applied mechanical work imposed on a volume of the TMJ disk. This is also known as energy density (mJ/mm^3). Biphasic modeling of contact mechanics has shown that energy density produced by plowing tractional forces is balanced by an internal strain energy in the collagen–glycosaminoglycan matrix, and pressurization of the interstitial fluid (1, 2).

Like all synovial joints, failure of the articulating tissues is thought to involve an interactive process between mechanical fatigue, oxidative stresses, and inflammation (3). The variables determining the rate of mechanical fatigue of articulating surfaces are the frequency, magnitude, and concentration of mechanical strains, and innate susceptibility of the tissue. Why destruction of the articular tissues occurs earlier in the TMJ compared to knees and hips may be due to these variables (4).

Current evidence suggests that fatigue of the TMJ disk may involve magnitude of joint loads and the consequent mechanical stresses and strains imposed on the tissue (5–8). Data reported by Iwasaki et al. (9) indicated that significant differences in joint loads exist among TMD diagnostic subgroups and suggest that there are unique mechanisms of cartilage failure within diagnostic subgroups. Magnitude and frequency of TMJ loads are likely to affect the rate of articular tissue mechanical fatigue. Equally important is the routine mechanical work imposed on cartilage due to tractional forces, which are a combination of frictional and plowing forces that occur when a stress-field moves over the surface and causes deformation of the cartilage matrix (10, 11).

The objective of the current project was to test the hypothesis that energy densities in the TMJs of subjects with bilateral disk displacement with and without pain were significantly higher than in individuals with normal joints and without pain.

Materials and methods

The protocols used in this project were approved by two university institutional review boards. Sixty-eight informed and consenting subjects participated in this study. Inclusion and classification of subjects were based on Diagnostic Criteria for TMD (DC/TMD) (12) and bilateral magnetic resonance images (MRI) of TMJs (13). Subjects with a history of frank trauma to the TMJ were excluded. According to jaw muscle or TMJ pain status (+P = presence of pain) and disk position (+DD = disk displacement), female ($n = 44$) and male ($n = 24$) subjects were categorized into three groups: +P+DD ($n = 16$; 15 females, one male; average age 34.9 years), –P+DD ($n = 16$; 12 females, four males; average age 33.6 years), and –P–DD ($n = 36$; 17 females, 19 males; average age 30.7 years).

Dynamic stereometry of the TMJ was used to estimate the magnitudes of the variables used in energy density calculations. The process required the three-dimensional software reconstruction of each subject's anatomical structures, captured from MRI, and the animation of these structures using motion-tracking data (14). MRI of each subject were made from serial oblique sagittal slices perpendicular to the main condylar axis of each TMJ using a 1.5 T MRI tomographic apparatus (Siemens Magnetom™; Siemens Medical Solutions USA, Inc., Malvern, PA, USA) with TMJ surface coils of 12 cm radius. During the process of scanning, each subject bit into a custom occlusal registration appliance that carried a head reference system (three contrast spheres) to enable integration of MRI with recordings from jaw tracking. Static recordings were produced while each subject was biting into the occlusal appliance, which carried a head reference system (Fig. 1). As well, motion recordings of the jaws (jaw tracking) were produced while each subject performed 10 symmetrical opening and closing movements. Motion tracking was possible using an opto-electronic system (Fig. 1). Two triangular target frames, carrying three non-collinear light-emitting diodes (LEDs) each, defined maxillary and mandibular coordinate systems. The target

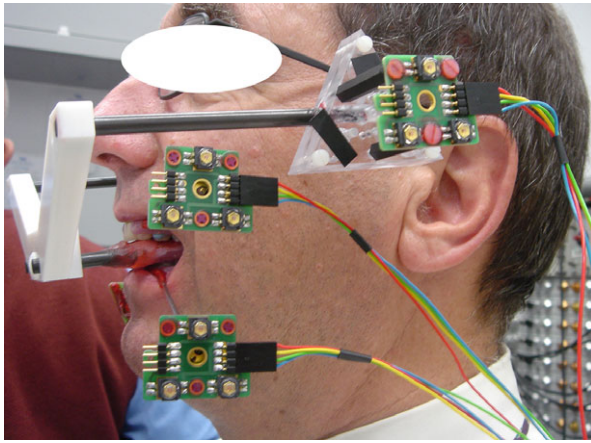


Fig. 1. Opto-electronic system for jaw tracking – three triangular target frames, carrying 3 non-collinear light-emitting diodes (LEDs) each, defined reference, maxillary and mandibular coordinate systems. The target frames for the jaws were fixed temporarily to facial surfaces of maxillary and mandibular canines and first premolars on one side by means of custom splints.

frames were fixed temporarily to vestibular surfaces of maxillary and mandibular canines and first premolars on one side by means of custom splints. The LEDs determined head- and mandible-related coordinate systems. The time-varying maxillary and mandibular LED positions were recorded by three linear cameras with fixed geometry and resolution of better than $5\ \mu\text{m}$ at a sampling frequency of 200 Hz. Motion of the lower jaw was calculated relative to the head; thus, head motion was eliminated.

Software reconstruction and animation of the TMJ were performed on a graphics workstation by means of custom software. MR scans were segmented for extraction and vectorial description of anatomical structures as well as for determination of the centers of the reference spheres. Segmentation of the anatomy was obtained first by tracing on each MR slice object contours defined by driving points of spline functions. To construct a software model from the MR slices in three dimensions, the contour sets were triangulated and the resulting surfaces were represented realistically by means of shading algorithms (Fig. 2). Resolution was improved by calculating interslice surface points and applying a smoothing algorithm. Animation of the TMJ was achieved by means of mathematical transformations, using the computer to calculate continuously the spa-



Fig. 2. TMJ Anatomy Reconstruction and Kinematics – anatomy of the TMJ (right-side fossa, condyle, and ramus shown from superior view) was reconstructed from MR slices. MR scans were segmented for extraction and vectorial description of anatomical structures as well as for determination of the reference common to MRI and jaw tracking. Animation of the TMJ was achieved by means of mathematical transformations, using the computer to calculate continuously the spatial positions of all vertices of polygons describing the recorded surfaces. Lines depict the jaw-closing paths of three landmarks: lateral pole of condyle (blue), condylion (green), and medial pole of condyle (red).

tial positions of all vertices of polygons describing the recorded surfaces. Tests of the system showed maximum errors of 0.9%.

Magnitudes of the variables of interest (aspect ratio, (a/h) ; compressive strain, $[\Delta h/h]$; linear distance (ΔD) and velocity (V) of stress-field translation; cartilage volume (Q)] for each subject were determined from the reconstructed and

animated MRI for each subject over 5 ms time intervals. The stress-field in the TMJ was located by finding the area of minimum condyle-fossa/eminence distance. For each sampling time of mandibular motion, the 30 smallest adjacent condyle-fossa/eminence distances, measured between polygon vertices, were identified. These distances were averaged to determine the minimum condyle-fossa/eminence distance or disk thickness, h . The centroid of the area defined by these 30 minimum distances was calculated and defined the mediolateral position of the stress-field, D . The standard deviation of the positions of the 30 minimum distances about the centroid was also calculated to determine the radius of the stress-field, a . The path of D was displayed graphically in a planar coordinate system representing the condylar surface. The mediolateral axis corresponded to the direction of the condylar long axis. The coordinates of the mediolateral position of D were smoothed over 30 ms, and velocity of the stress-field translation (V , mm/s) calculated for each jaw-closing movement. Volume of cartilage (Q , mm³) under the leading edge of the translating stress-field was also measured. The magnitudes of these variables were used in an empirically derived equation (15) and the results employed to determine instantaneous mechanical work and energy densities in the right and left TMJs of each subject during the jaw-closing movement.

The calculation of TMJ tractional forces (F_{traction}) required an estimation of the subject-specific TMJ normal (perpendicular) forces (F_{normal}). To accomplish this, a computer modeling approach was used. The modeling method has been described (9, 16, 17). Briefly, each subject's three-dimensional craniomandibular geometry (Fig. 3) was developed from standardized cone-beam computed tomography images. Bilateral sagittal effective eminence shapes were characterized via dynamic stereometry. These data were used in a numerical model, which employed an objective function of minimization of the sum of muscle forces squared to predict contralateral (left) condyle loads consequent to 20 N vertical and non-vertical loads applied to the mandibular canine.

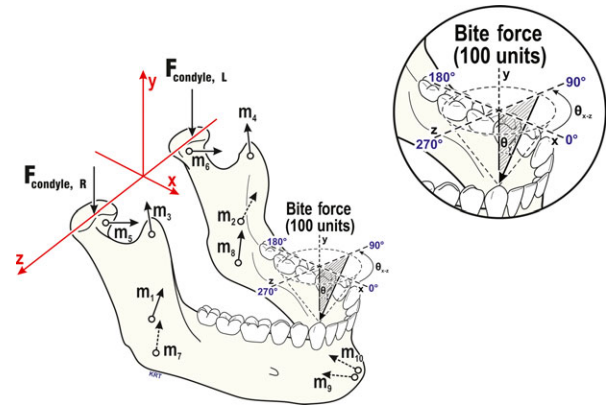


Fig. 3. Craniomandibular geometry used in numerical modeling of jaw loading – the axis system and force vectors involved are illustrated for biting at right canine. The force vectors based on individual subjects' anatomy included: TMJs (F_{condyle} ; R = right, L = left), and muscles representing five muscle pairs ($m_{1,2}$ = masseter, $m_{3,4}$ = anterior temporalis, $m_{5,6}$ = lateral pterygoid, $m_{7,8}$ = medial pterygoid, $m_{9,10}$ = anterior digastric muscles). Bite forces were modeled to mimic *in vivo* biting conditions, characterized by angles in the occlusal plane (θ_{xz} , 0–350°, illustrated above occlusal plane, and relative to vertical (θ_y , 0–40° shown as shaded, where 0° is normal to the occlusal plane). All TMJ and muscle forces required for static equilibrium were expressed relative to the 100-unit applied bite force.

Load vectors ranged from 0° to 40° from vertical (θ_y , Fig. 3), with azimuth plane angles (θ_{xz}) ranging from 0° to 350°. Computer model-predicted contralateral F_{normal} were averaged for a given subject.

Data collected from individual subjects were input to the empirically derived equation (15) describing the relationship between stress-field geometry and dynamics, and a tractional coefficient ($f = F_{\text{traction}}/F_{\text{normal}}$). Tractional force (F_{traction}) estimates were then determined using the product of the tractional coefficient and average contralateral TMJ forces for the subject ($F_{\text{traction}} = f \times F_{\text{normal}}$) and used in work and energy density calculations for each of 10 jaw-closing movements. Instantaneous mechanical work done (W , mJ) was calculated continuously over 5 ms intervals during cyclic movement of the mandible by the equation:

$$W = F_{\text{traction}} \cdot \Delta D$$

Instantaneous energy density calculations over 5 ms time intervals during cyclic movement of the mandible were accomplished using the equation:

$$\psi = (F_{\text{traction}} \cdot \Delta D)/Q$$

The energy densities for the 10 jaw-closing movements were averaged for each subject, and then diagnostic group means were calculated. Analysis of variance, followed by Tukey–Kramer post hoc analyses tested for significant diagnostic group differences (adjusted $p < 0.05$) in mean energy densities for jaw closing.

Results

Among all subjects, average energy densities for 10 jaw-closing movements ranged from 0.1 to 81.6 mJ/mm³. Among diagnostic groups, mean energy densities for jaw closing (\pm standard error) were 12.7 ± 1.5 mJ/mm³ for the +P+DD group, 7.4 ± 1.4 mJ/mm³ for the –P+DD group, and 5.8 ± 0.9 mJ/mm³ for the –P–DD group. Mean energy densities for the +P+DD group were significantly higher compared to –P+DD ($p = 0.034$) and –P–DD ($p = 0.0006$) groups (Fig. 4), while those for the –P+DD and –P–DD groups were not significantly different ($p = 0.61$).

Discussion

Due to the lack of vascularity of the TMJ disk, the movement of solutes throughout the TMJ disk

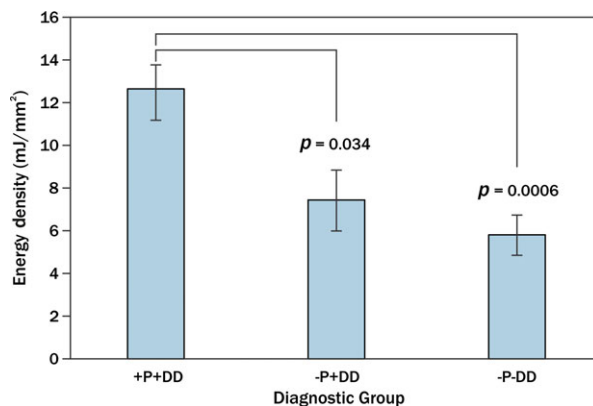


Fig. 4. TMJ energy densities in three TMD diagnostic groups – mean energy densities for subjects with (+) and without (–) pain (P) and disk displacement (DD) are shown, where vertical lines indicate standard errors above and below the means. Results for the +P+DD groups were significantly higher compared to –P+DD ($p = 0.034$) and –P–DD ($p = 0.0006$) groups.

matrix is determined by osmotic pressure for fluid absorption, and mechanical loading for exudation. Higher cell density and nutrient consumption rates in the TMJ disk, compared to hyaline cartilage and the intervertebral disk, make the TMJ disk fibroblasts vulnerable to oxidative stress (3, 18). Stress-field translation-related plowing forces (2, 15) move fluids through the disk to ensure adequate nutrition to disk fibroblasts. However, energy densities of sufficient magnitude potentiate the fatigue of the collagen fibers of the disk. The significantly higher energy densities in +P+DD subjects may be a unique contributing mechanism for mechanical fatigue of the TMJ, which resulted in the disk displacement in this diagnostic subgroup.

Although there were no significant differences in energy densities between –P+DD and –P–DD subjects, the trend to slightly higher values in –P+DD subjects likely reflected the effect of higher TMJ loads in –P+DD subjects. Previous work reported that during normal function, TMJ loads in –P+DD subjects were 40–60% higher for similar biting conditions compared to +P+DD and –P–DD subjects (9). In addition, new data suggest that frequency of loading may be different among diagnostic groups; specifically, there is evidence that chronic low-level loading of the mandible is more prevalent in –P+DD women (19, 20). Given group differences in contact mechanics, and differences in loading behaviors, it is possible that distinct variables contribute to fatigue of TMJ disks in TMD diagnostic subgroups.

A limitation of the current study is that no analyses of gender effects could be conducted because of the lower frequency of male compared to female participants in the +P+DD and –P+DD groups. Whether or not the number of males in the –P–DD group may have contributed to significantly lower energy densities of the diagnostic group requires further scrutiny. Future studies are needed to investigate gender differences in TMJ energy densities. In addition, longitudinal follow-up of currently healthy individuals with relatively high and low energy densities could reveal whether or not these individuals have different risks for development of TMD.

Conclusions

Diagnostic group differences in mechanical energy densities suggest that mechanical work in general, and energy density (mJ/mm³) specifically, may be a unique mechanism of cartilage fatigue in TMD subjects with pain and disk displacement.

Clinical relevance

Articular cartilage failure may be related to a mechanical fatigue process. The precocious development of degenerative joint disease of the TMJ, compared to post-cranial joints such as the knee, may be due to a unique mechanism, which

concentrates mechanical work per unit volume of the TMJ disk during normal function. The findings of this study suggest that in patients with myofascial or TMJ pain and bilateral disk displacement, average energy densities are more than twice those seen in healthy individuals and may be a unique mechanism contributing to cartilage fatigue in this TMD diagnostic subgroup.

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